

The effect of volume fraction on the fatigue strength of unsaturated polyester / glass fiber composite

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Abstract

In this work polymeric composites were done from unsaturated polyester as a matrix reinforced with glass fiber type (E-glass) with two different volume fraction 20% & 40%. Fatigue tests showed that the number of fatigue cycles to failure limit for samples reinforced with uniform (woven Roving 0-90°) E-glass fiber and random (continuous fibers) with volume fraction 40% more than that for the same samples with volume fraction 20%. Also the fatigue results showed that the uniform samples failed with fatigue cycles more than that of random.

Key words

volume fraction,
fatigue strength,
unsaturated polyester /
glass fiber composite.

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تأثير الكسر الحجمي على قوة الكلالة لمتراكب البولوي استر غير المشبع / ألياف زجاجية

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الخلاصة

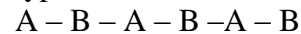
تم تصنيع مادة متراكبة ذات أساس من راتنج البولوي استر غير المشبع المدعم بالألياف الزجاجية من نوع (E-glass) المنتظمة (0 – 90°) والعشوائية بكسرين حجمين (20% , 40%)، وتعرضها لفحص الكلال. لقد تم من خلال النتائج العملية ان عدد دورات الكلال لحد الفشل للعينات المنتظمة والعشوائية عند كسر حجمي 40% أكبر من عدد دورات الكلال لنفس العينات عند كسر حجمي 20%، وأوضحت النتائج أيضاً أن عدد دورات الكلال للعينات المنتظمة تفشل بعدد أكبر من عدد دورات الكلال للعينات العشوائية.

Introduction

A composite may be defined as any multiple phase material that exhibits a significant proportion of the properties of both the constituent material, a judicious combination of properties[1].

The properties that can be improved by forming a composite material include high strength, weight, wear resistance, corrosion resistance, stiffness, fatigue life and thermal conductivity [2].

The term "polyester" resin is applied to the condensation reaction products of dicarboxylic acids and diols (glycols). There are therefore, strictly alternating polymers of the type shown below[3]:



Unsaturated polyesters resins have excellent mechanical and chemical properties, good chemical and weather resistance, good electric, resistance to light, low cost [4].

Glass fiber reinforced polyester composites are used extensively in building and construction, transportation, electric industries and in domestic application [5].

Fatigue is the failure or decay of mechanical properties after repeated application of cyclic stress [6, 7]. Fatigue life is defined as the total number of stress cycles to cause failure at limit stress level [8]. The fatigue properties of composite material depend on factors as the interaction between the mechanical properties of the matrix and the reinforcement, the strength of the bond between the two, the volume or weight fraction of type of loading, the loading frequency and the temperature [9]. There are five major damage mechanisms matrix cracking, fiber breaking, crack coupling, delaminating beginning and delaminating growth [10].

Freire [11] investigated the damage mechanism and fracture prevention in E-glass polyester resin composites, his work was limited to bidirectional and stacked bidirectional woven fabric textile. Husain [12] studied composite materials formulated by stacking four layers of fiber glass indifferent angle orientations immersed in polyester resin. These were tested under dynamic load in fully reversible tension-compression tests as fatigue testing. Hayder [13] studied experimental and theoretical investigation into some mechanical properties of glass polyester composite under static and dynamic loads. Hind [14] studied fatigue properties for polyester and epoxy resins reinforced with glass fiber.

Experimental

1. Material used

1. Unsaturated polyester (Siropol 8341) manufactured by Saudi Arabic Co. as a matrix material which solidified by addition its hardener (mekp) methyl / Ethyl / Kenton peroxide with ratio 2gm to 100gm

from unsaturated polyester at room temp. Table 1 showed the properties of unsaturated polyester.

2. Glass fiber type (E-glass) as a reinforced material with density 2-58 gm/cm³.

2. Sample preparation

Hand Lay-up produced was used for preparation of the sample, because this way is easy, simple and cheap. This method includes:

1. Cutting up many laminates of fiber glass type (E-glass) random and woven roving with dimensions (20×20)cm.
2. Weigh the glass fibers by sensitive balance (0.0001 gm).
3. The weight and volume of matrix including UP and hardener were known after knowing the weight and volume of fiber glass from the relation of volume fraction of fiber glass as follow:

$$\phi_f = \frac{V_f}{(V_f + V_m)} = \frac{V_f}{V_c}$$

where ϕ_f = the volume fraction of glass fiber

V_m = volume of matrix (polyester and hardener)

V_f = volume of fiber

V_c = volume composite matrix

$$V_c = V_f + V_m$$

4. Mixing the Unsaturated polyester and hardener very well to get homogeneity.
5. Pour some resin on the glass slate which covered with wax. Then put fiber sheet on the resin. After that putting some resin on the surface of fiber glass to cover it very well. The second glass fiber sheet put on the first one loading with suitable load.
6. After (24) hours the sample removed from glass slates and cured in dry oven (6h with 60°).
7. Cutting up the samples as in Table 2 with length (100 mm) and width (10 mm) for

all samples, the thickness depends on the number of layers in the sample.

8. Make a hole in each sample with diameter (4 mm) at one edge with

distance (3 mm) from the ribs, to connect the sample to device for the purpose of tests Fig. 1.

Table 1 : The physical properties of unsaturated polyester resins (UPE).

UPE	density ρ (g/cm ³)	Young modulus E (MPa)	Tensile strength σ (MPa)	Thermal conductivity K ($\frac{W}{M.K}$)
	1.2 – 1.5	2000 – 4500	40 – 90	0.2

Table 2 : The type and number of reinforcing Layers of samples for unsaturated polyester/fiber glass composite.

No. of samples	Type of samples	Thickness (t) mm	Length L (mm)	Width d (mm)
M 1	Pure	1.25	100	10
M 2	UPE + 1 Un G.f	1.44	100	10
M 3	UPE + 2 Un G.f	1.61	100	10
M 4	UPE + 1 Ra G.f	1.39	100	10
M5	UPE + 2 Ra G.f	1.57	100	10



Fig .1: Prepared samples

manufactured by Hi-tech British company (Fig. 2) to test the fatigue performance for all samples. by applying alternating or fluctuating bending to a cantilever strip or material.



Fig .2 alternating bending fatigue machine

3. Instrumentations used

3.1.Alterbending Bending fatigue machine

In this work we used the alternating bending fatigue machine which

Results and Discussion

Fatigue tests were done for samples of pure unsaturated polyester and for reinforced samples. The results for volume fraction 20% and 40% for uniform and random fibers distribution showed in Tables 3 and 4 respectively. Table 3, shows that the

pure sample of (UP) failed with fatigue cycles (5820) at load (4.5)N and deflection (5)mm. These cycles are less than that for reinforced samples, because (UP) have fast solidification after curing [15].

Table (3) : The load, deflection and the number of cycles for unsaturated polyester samples (un Reinforcing and reinforcing with glass fiber at volume fraction 20%.

Sample No.	Type	Load P (N)	Deflection δ (mm)	No. of cycles N
M 1	Pure	4.5	5	5820
M 2	UPE + 1 Un G.f	6	18	1107580
M 3	UPE + 2 Un G.f	12	10	921044
M 4	UPE + 1 Ra G.f	5.5	18	1×10^6
M 5	UPE + 2 Ra G.f	11.0	10	823142

Table (4) : The load, deflection and the number of cycles for unsaturated polyester samples (un Reinforcing and reinforcing with glass fiber at volume fraction 40%.

Sample No.	Type	Load P (N)	Deflection δ (mm)	No. of cycles N
M 1	Pure	4.5	5	5820
M 2	UPE + 1 Un G.f	7	18	1634144
M 3	UPE + 2 Un G.f	13	10	1131608
M 4	UPE + 1 Ra G.f	6.5	18	1485000
M 5	UPE + 2 Ra G.f	12	10	901202

Fig.3 shows that the samples reinforced with one layer of uniform glass fiber at volume fraction 20% failed with fatigue cycles (1107580) at load 6 N and deflection 18 mm, when we compared this sample with the same sample at volume fraction 40%, we found it failed with fatigue cycles(1634144) at load 7 N and def 18 mm. This belongs to the reason that the tensile strength of the composite sample increased

with increasing volume fraction[16].

Fig.3 showed the samples reinforced with two layer of uniform glass fiber at volume fraction 20% failed with fatigue cycles (921044) at load 12 N and def. 10 mm, while this sample at volume fraction 40% failed with fatigue cycles (1131608) at load 13 N and deflection 10 mm for the same above reasons.

Fig.4 shows the results of pure samples and reinforcing samples with random glass fiber. We noticed from the Fig.4 that the samples reinforced with one layer of random glass fiber with volume fraction 20% failed with fatigue cycles (1×10^6) at load 5.5 N and def. 18 mm, but when we compared this sample with the same sample at volume fraction (40%), we

found it failed with fatigue cycles (1485000) at load 6.5 N and def. 18 mm, Also the same results for two layers.

By comparing Fig.3 and 4, we noticed that the fatigue cycles decrease with increasing the number of reinforcing layers for all samples (random or uniform), also fatigue cycles at volume fraction 20% less than that at volume fraction 40%.

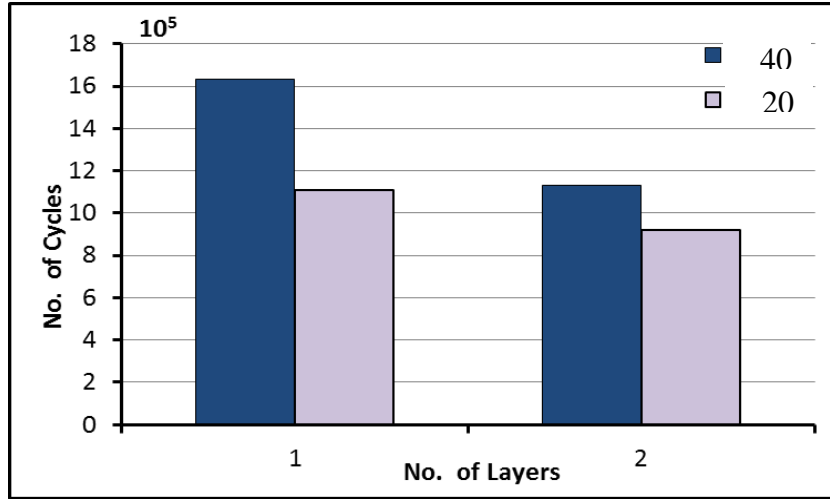


Fig.3: The relation between fatigue cycle and number of layer for uniform glass fiber at volume fractions 20% and 40%.

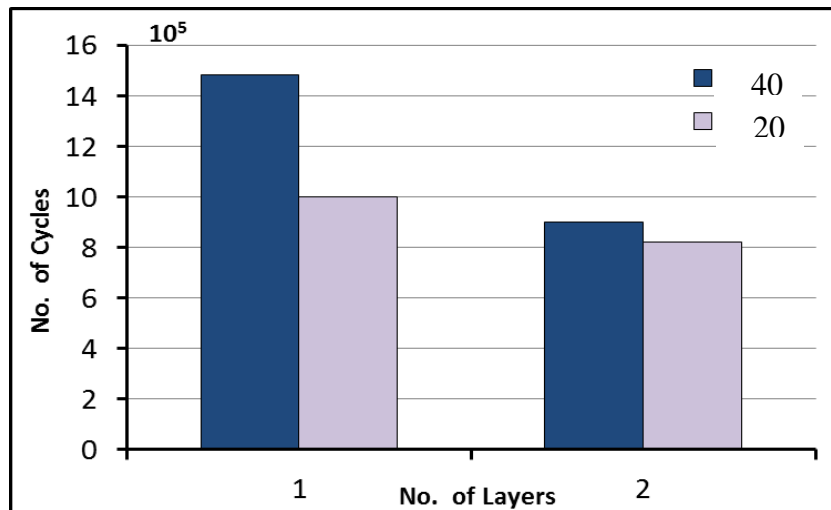


Fig.4: The relation between fatigue cycle and number of layer for random glass fiber at volume fractions 20% and 40%.

Conclusions

1. All samples with volume fraction 40% have fatigue strength more than that for samples with volume fraction 20%.
2. Fatigue cycles to failure decreases with increasing the number of reinforcing layer.

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